

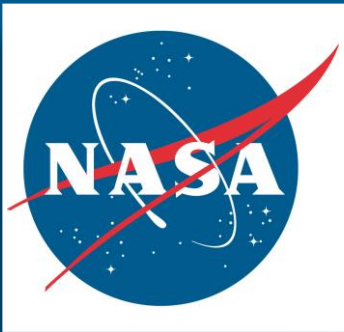
# THE EFFECT OF MICROSTRUCTURAL HETEROGENEITY ON DUCTILE FAILURE

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13TH US NATIONAL CONGRESS ON COMPUTATIONAL MECHANICS



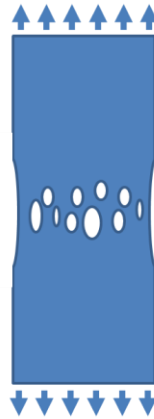
# DUCTILE FAILURE



Nucleation



Growth



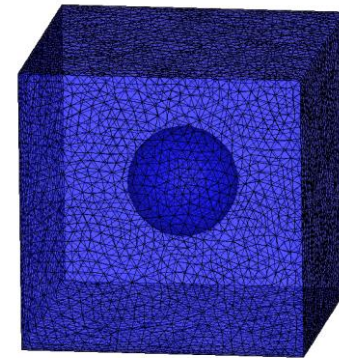
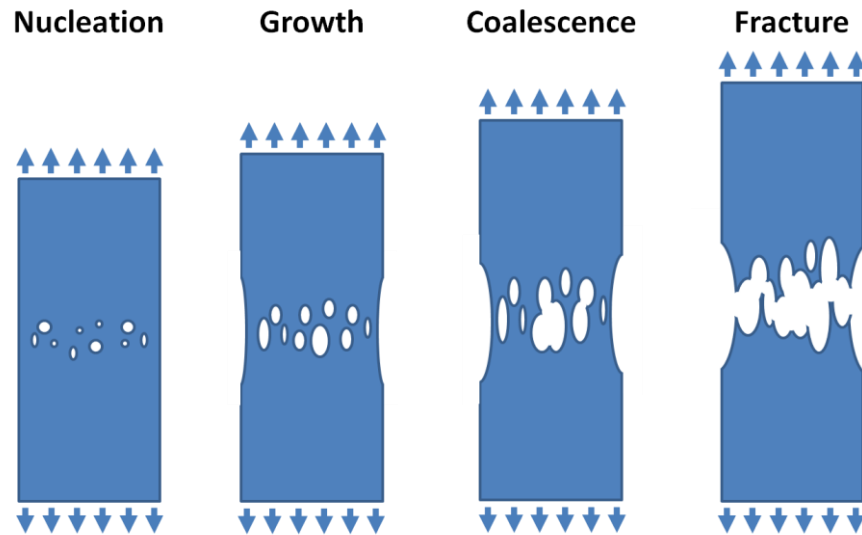
Coalescence



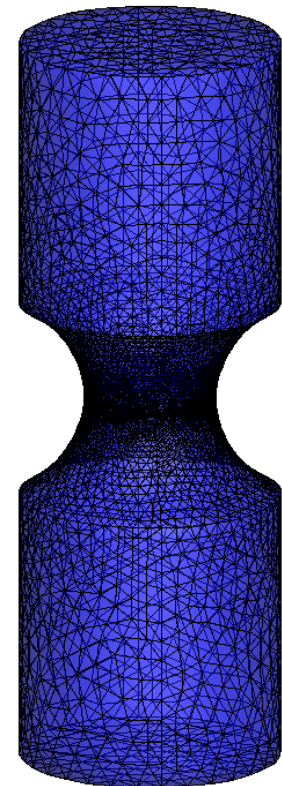
Fracture



# THE TWO SCALE PROBLEM



Micro



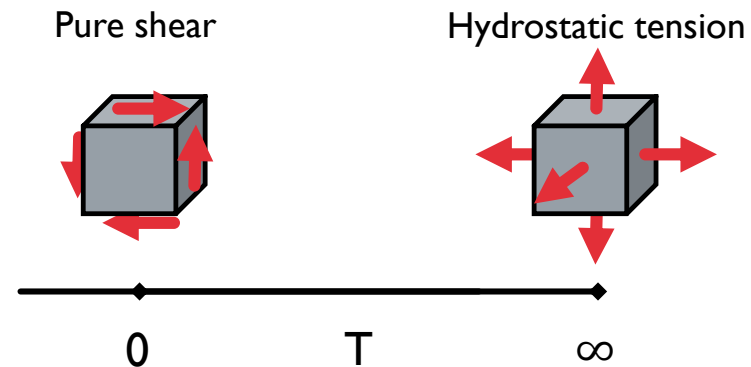
Macro

- Large-scale phenomenon controlled by micro-scale features
- We aim to capture two effects:
  - Variability in loading (micro-scale)
  - Variability in initial microstructure

- Here loading is defined by 2 parameters

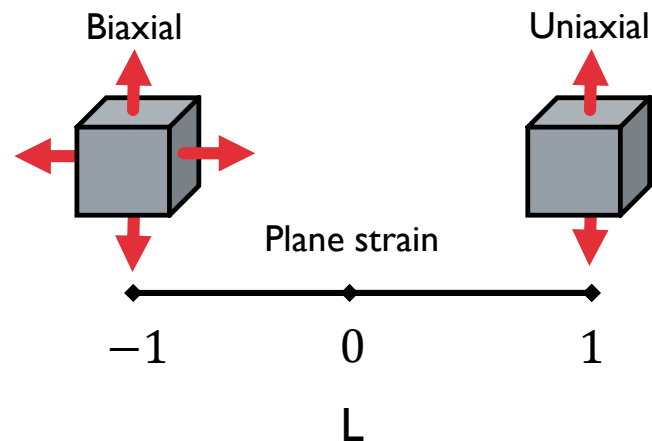
- Triaxiality

- $T = \frac{\sigma_h}{\sigma_e}$

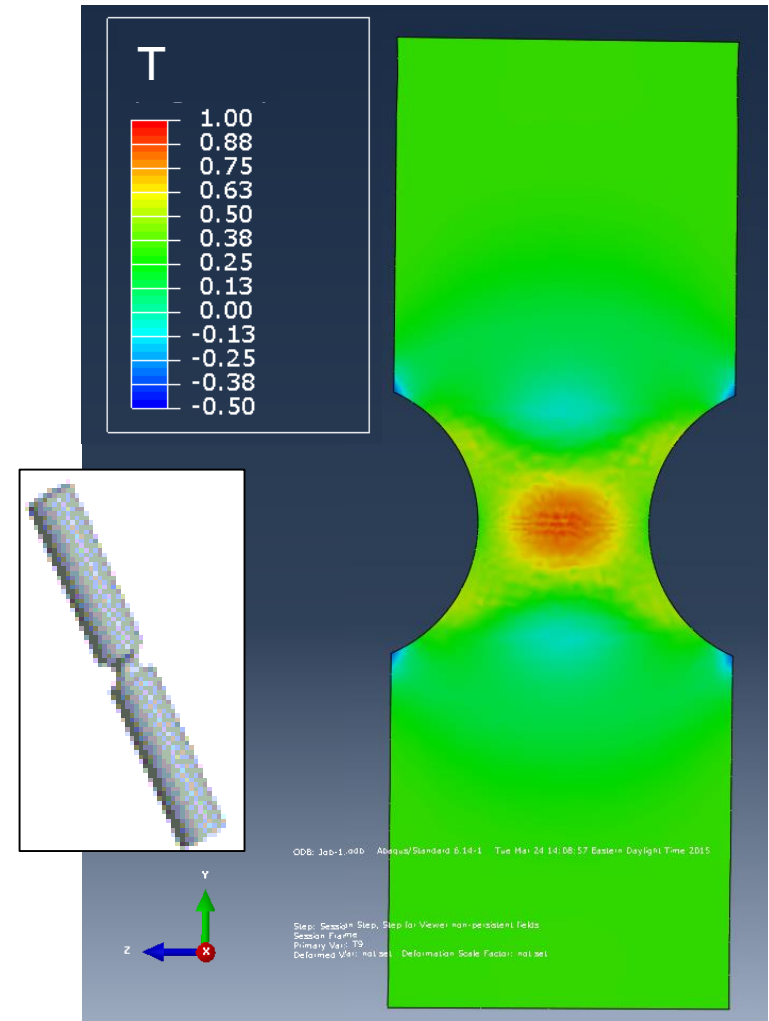
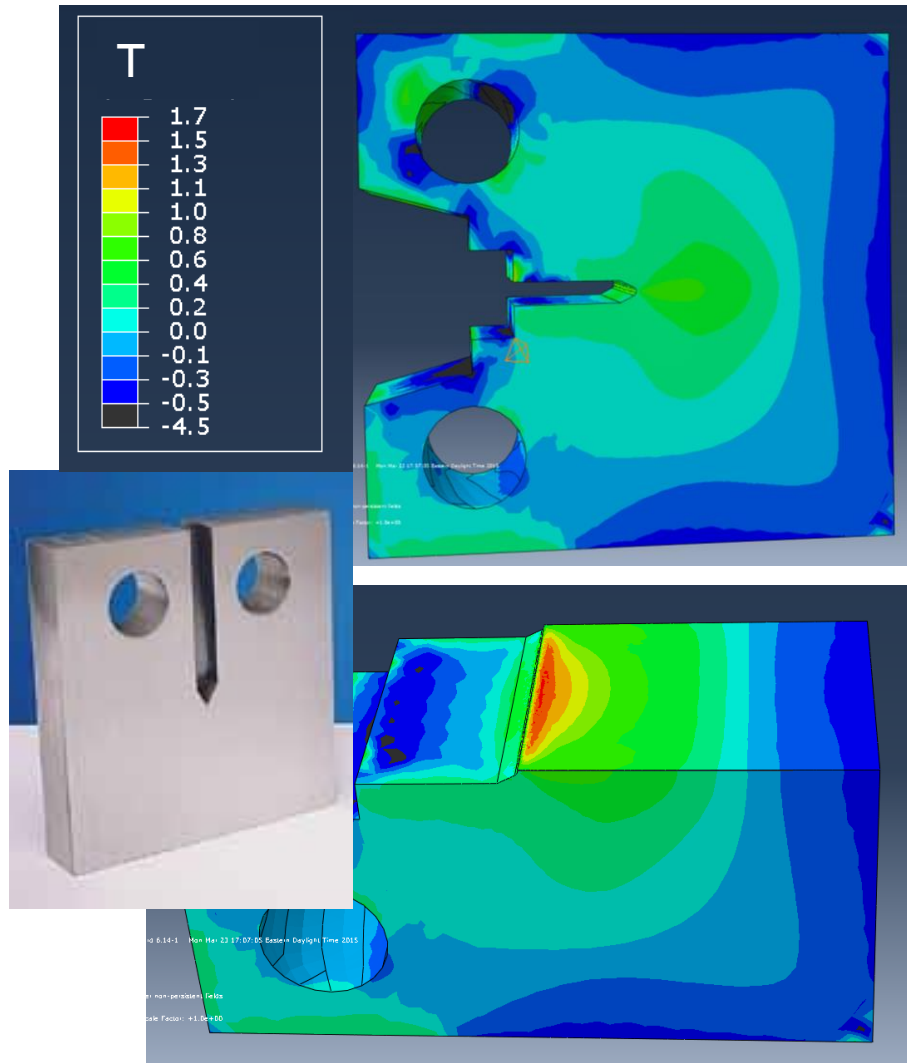
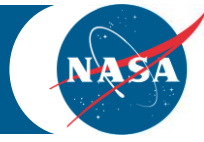


- Lode Parameter

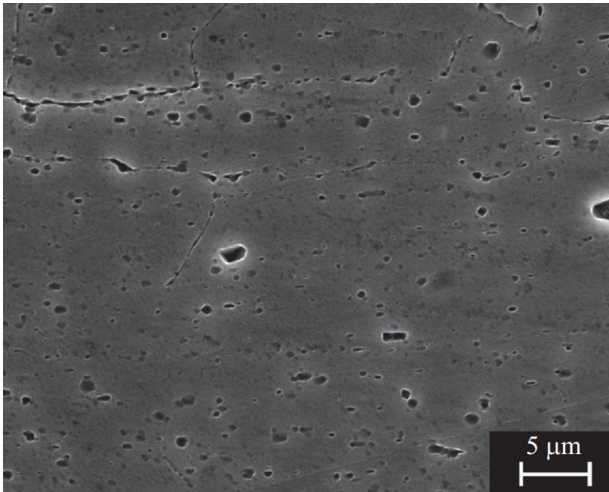
- $L = \frac{27J_3}{2\sigma_e^3}$



# VARIABILITY IN LOADING (MICRO-SCALE)

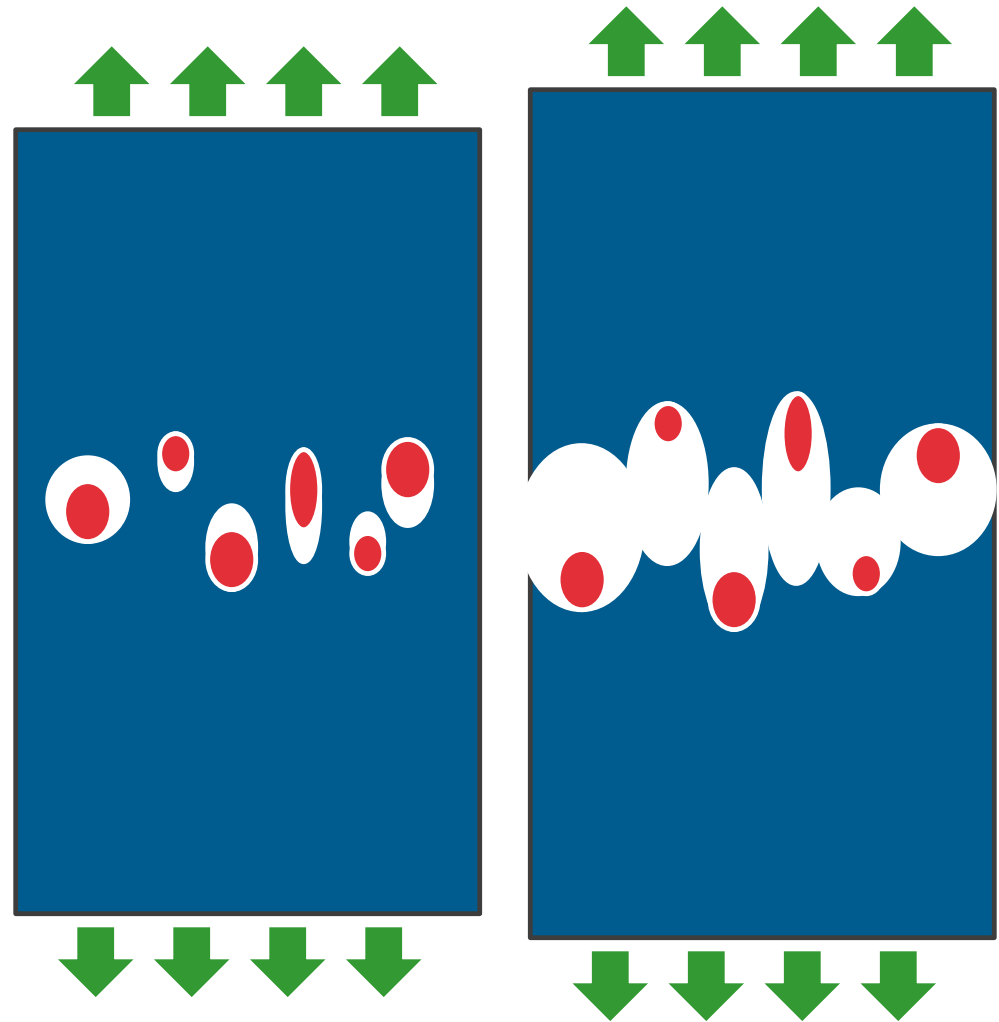


# VARIABILITY IN MICROSTRUCTURE



Chen and Lai (2014)

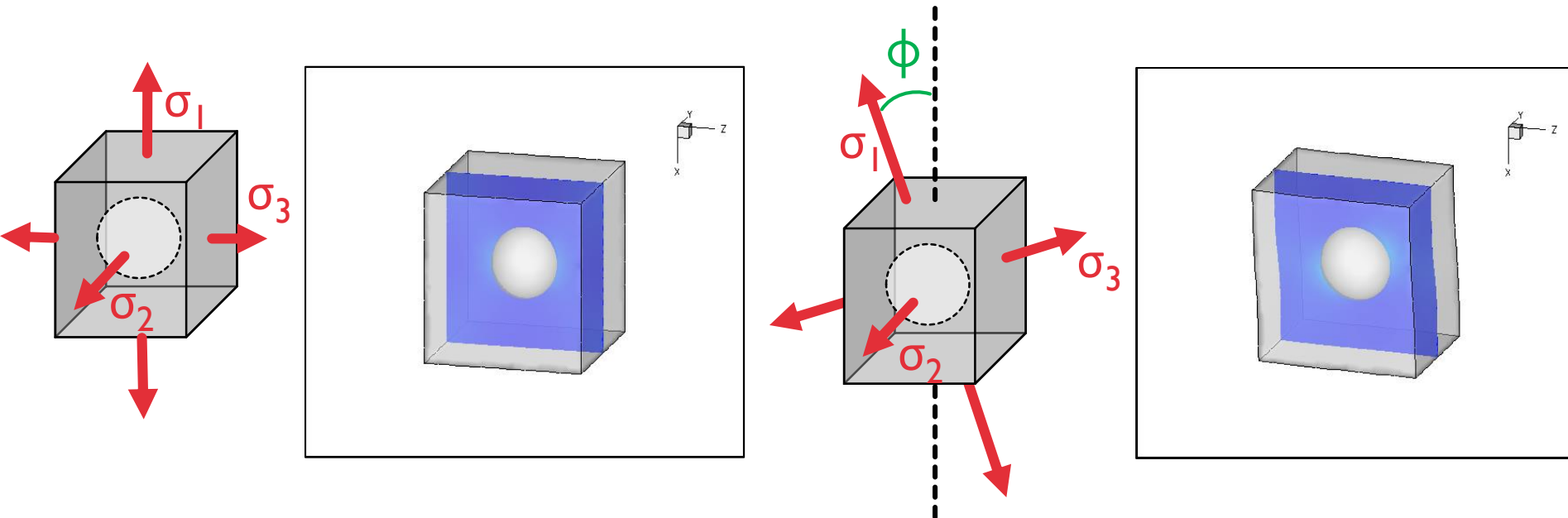
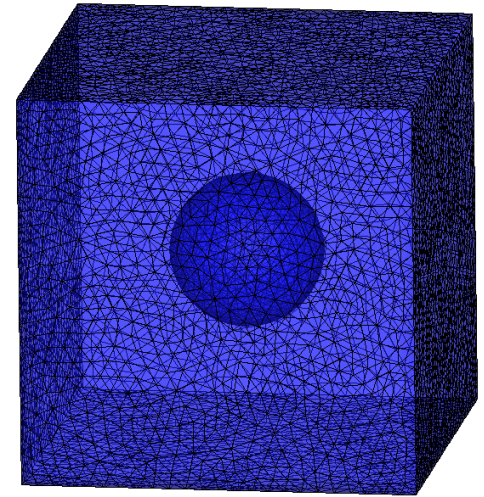
- Assume second phase particles act as voids
- Assume local porosity to be the defining microstructural feature



# THE MODEL: MICRO-SCALE



- 3D FEM
- Initial porosity ( $f_0$ ) defines geometry
- $T$  and  $L$  define the loading ratios:  $\frac{\sigma_2}{\sigma_1}$  and  $\frac{\sigma_3}{\sigma_1}$
- Allow for different localization modes



# THE MODEL: CONTINUUM-SCALE



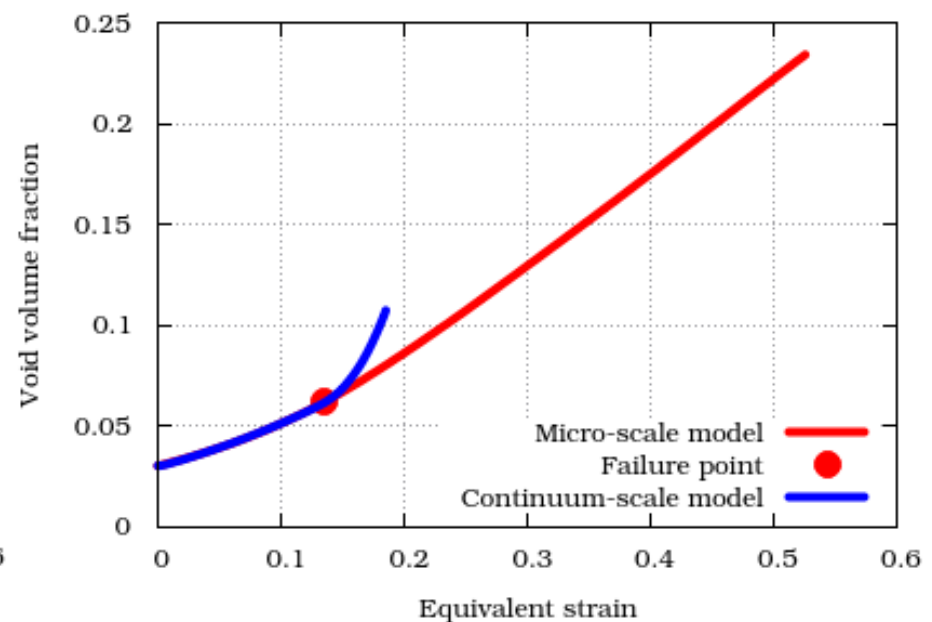
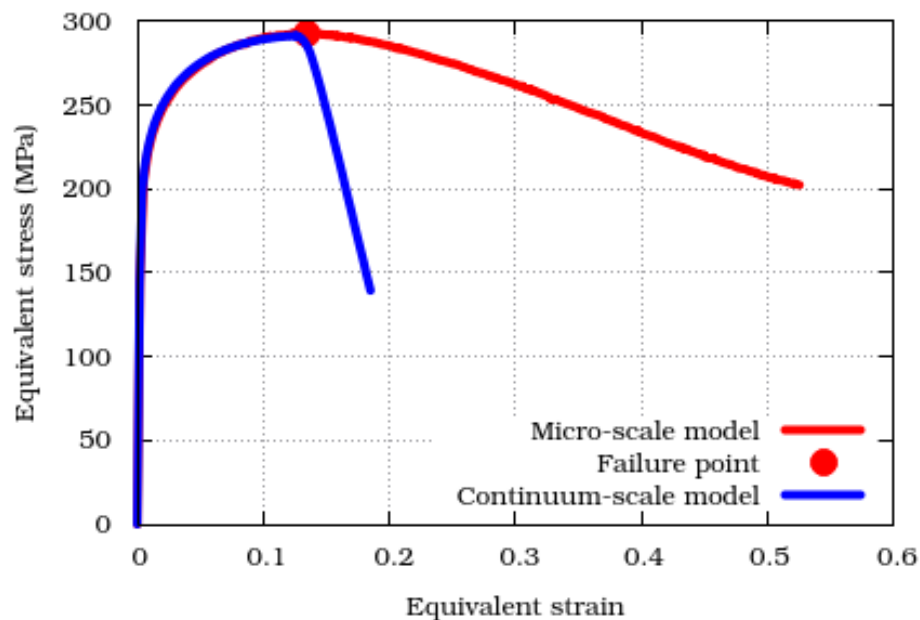
$$\Phi = \left( \frac{\bar{\sigma}}{\sigma_y} \right)^2 + 2q_1 f^* \cosh \left( \frac{3}{2} q_2 \frac{\sigma_h}{\sigma_y} \right) - (1 + q_1 f^*)^2$$

$$f^* = \begin{cases} f & : f \leq f_c \\ f_c + \kappa(f - f_c) & : f > f_c \end{cases}$$

$q_1$

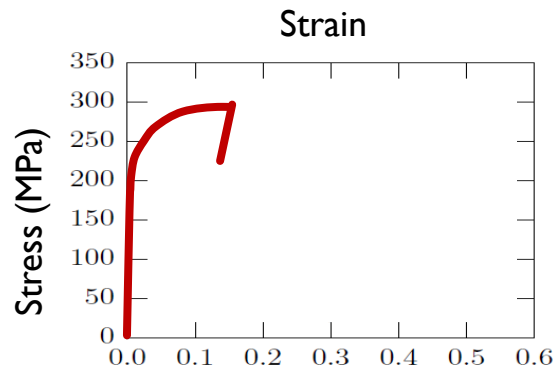
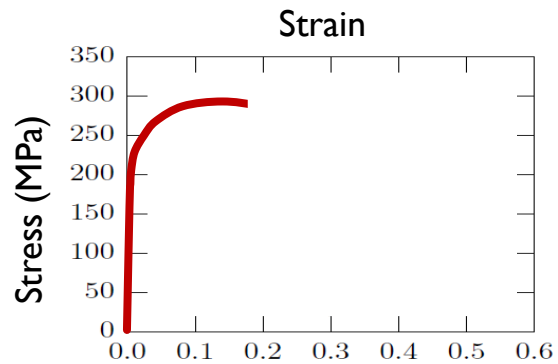
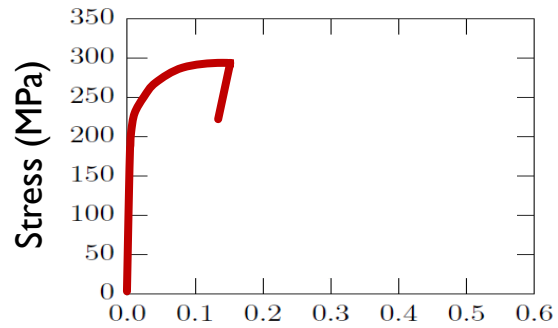
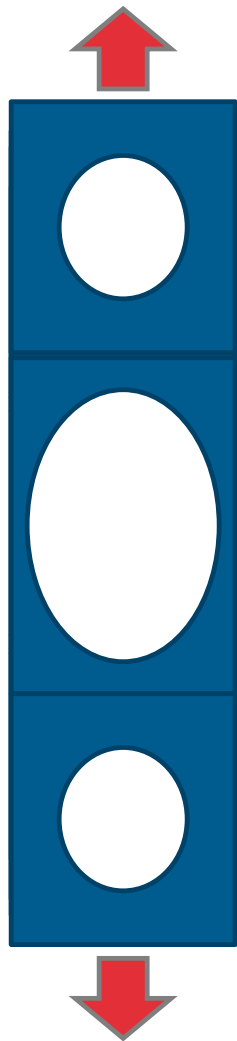
$q_2$

$f_c$

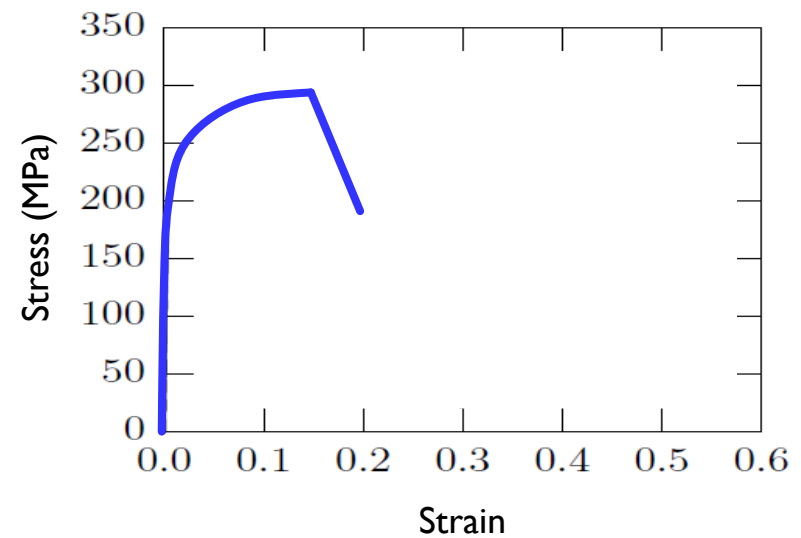




# POST-FAILURE RESPONSE



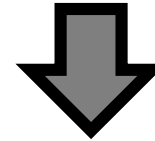
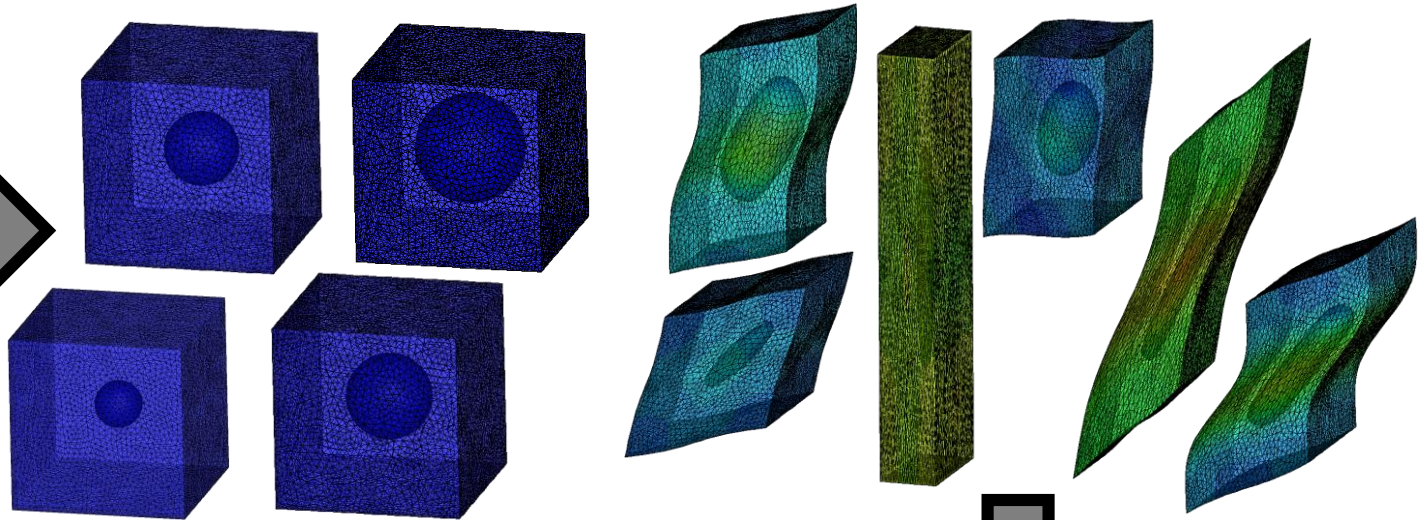
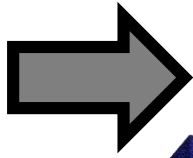
## Composite



# RECAP ON MECHANICAL RESPONSE



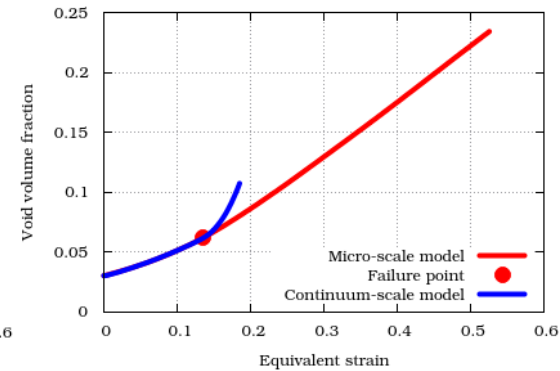
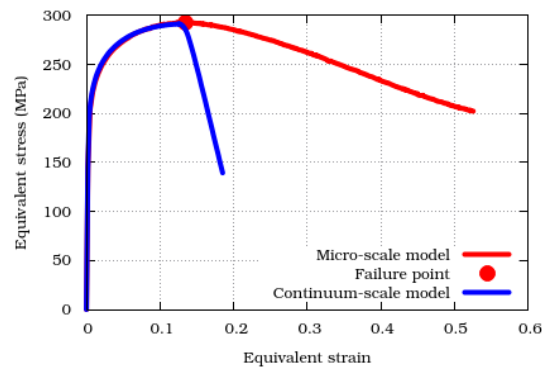
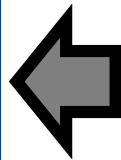
Given:  
 $f_0, T, L$



Response =  $f(\text{microstructure}, \text{loading})$

$q_1(f_0, T, L)$   
 $q_2(f_0, T, L)$   
 $f_c(f_0, T, L)$

$q_1$   
 $q_2$   
 $f_c$

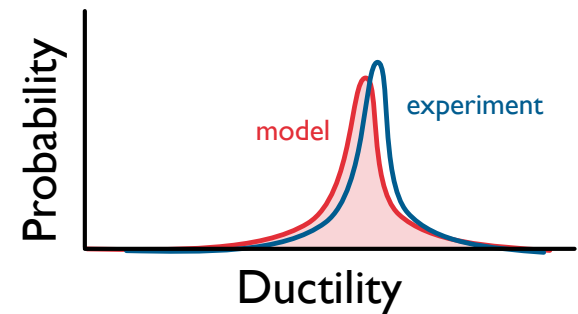
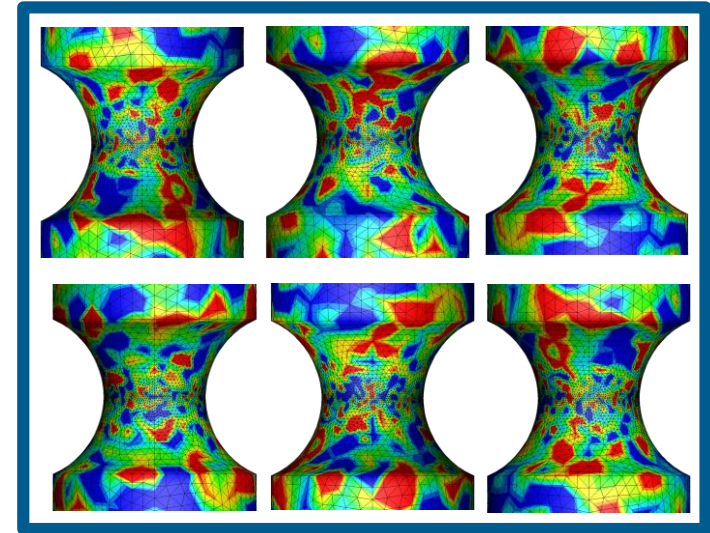
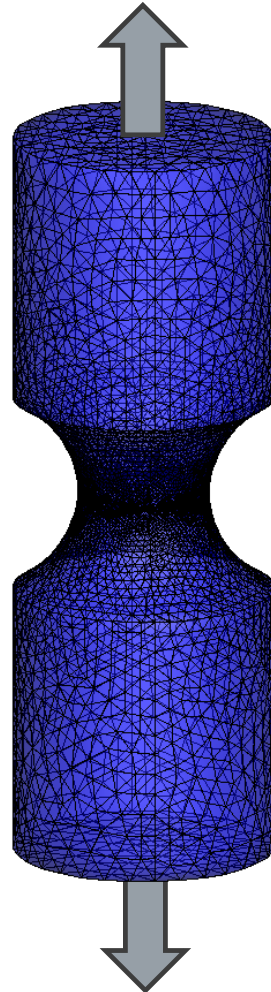
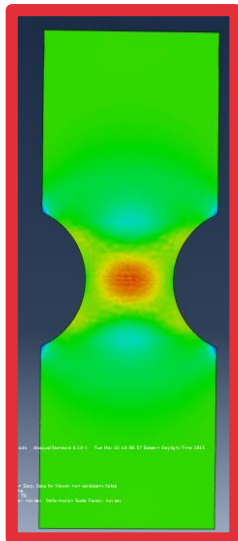


# UNCERTAINTY QUANTIFICATION

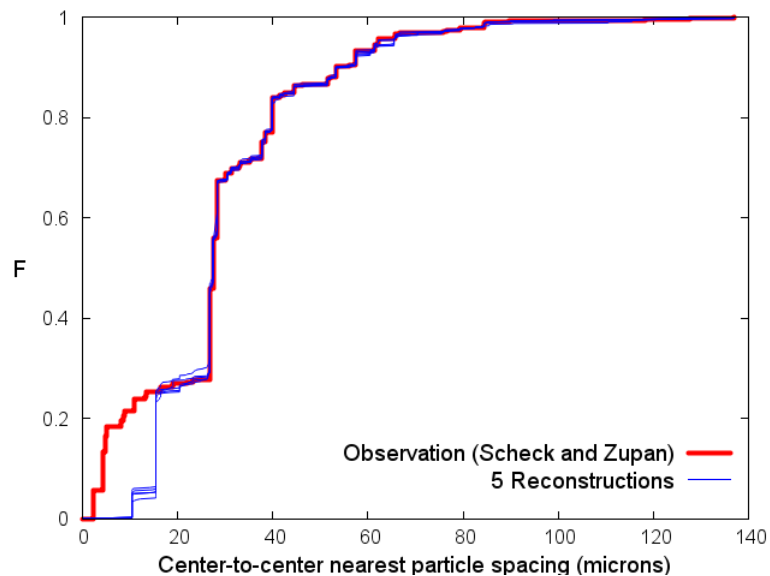
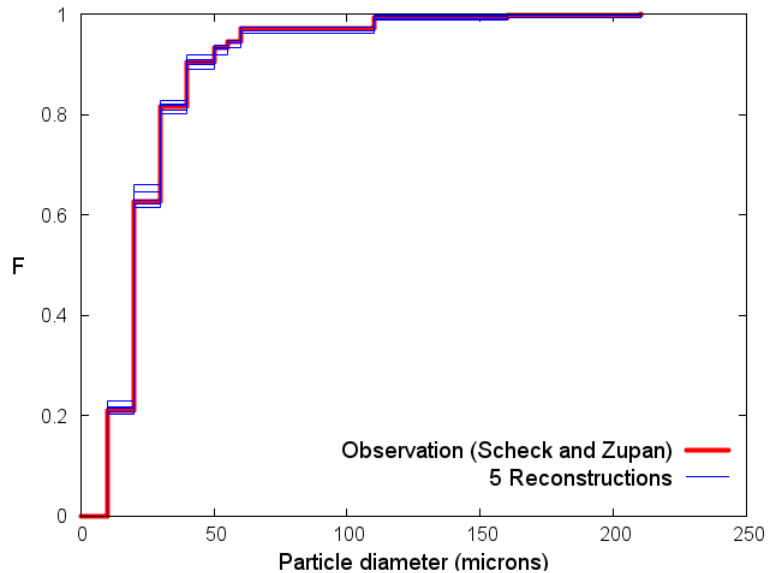


Response =  $f(\text{microstructure}, \text{loading})$

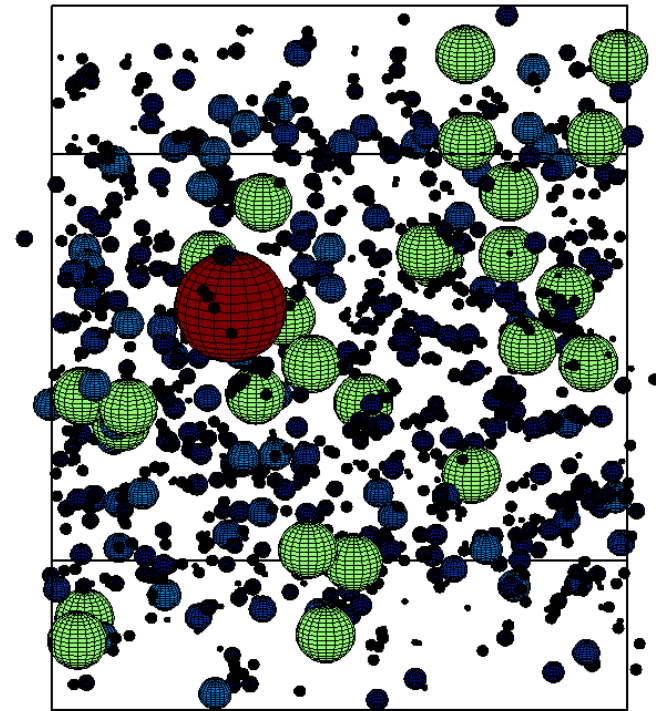
$$\begin{matrix} q_1(f_0, T, L) \\ q_2(f_0, T, L) \\ f_c(f_0, T, L) \end{matrix}$$



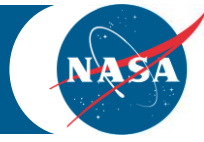
# CREATION OF REPRESENTATIVE MICROSTRUCTURES



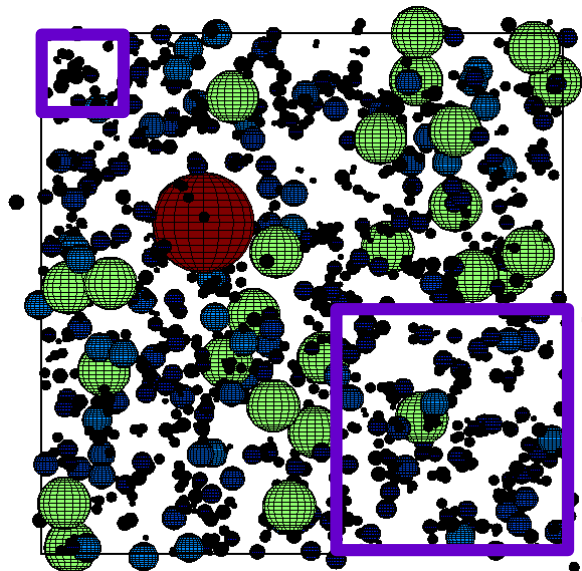
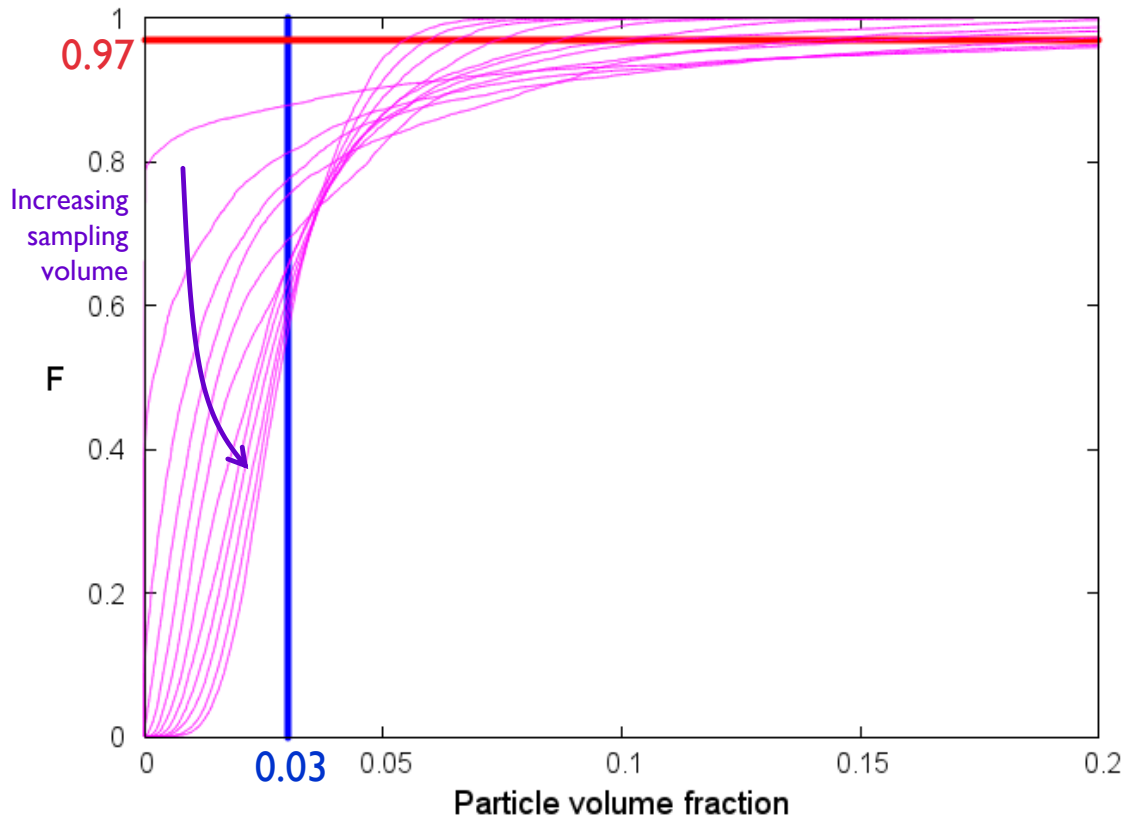
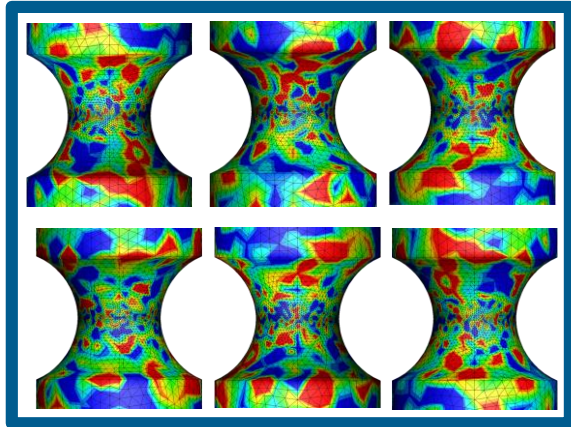
Average particle volume fraction = 3%



# QUERY RECONSTRUCTIONS FOR NEW STATISTICS

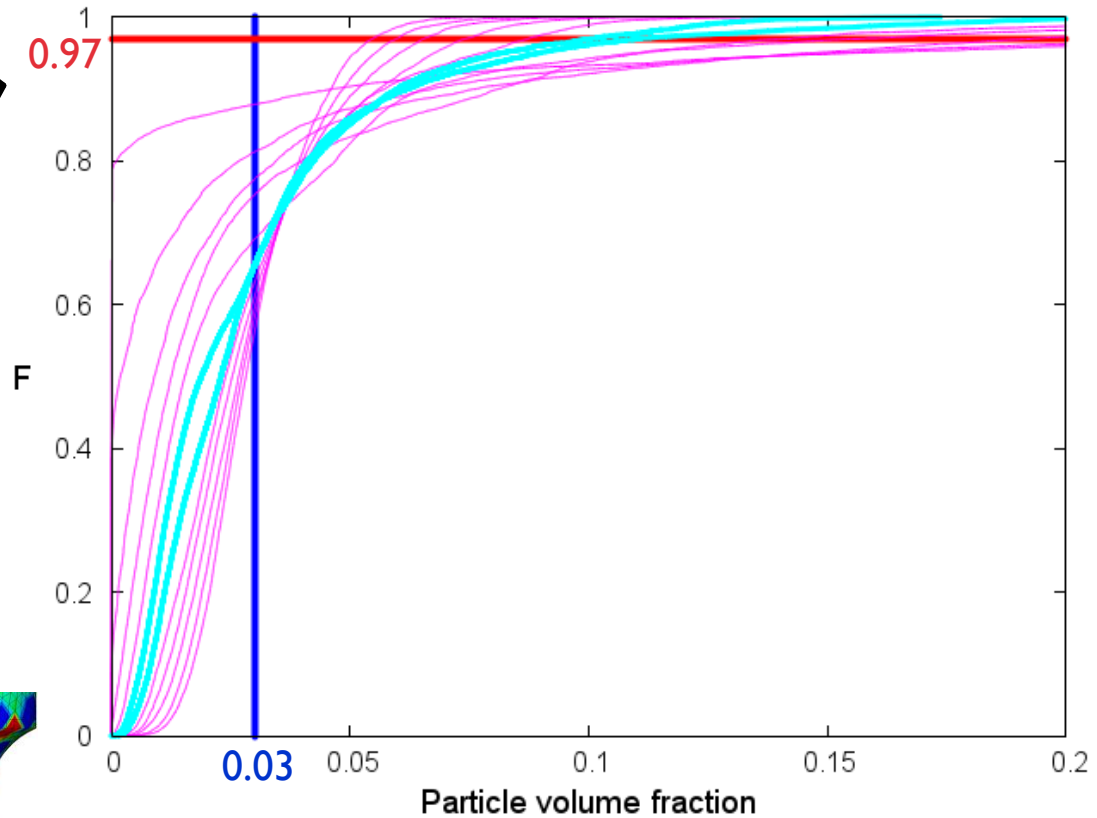
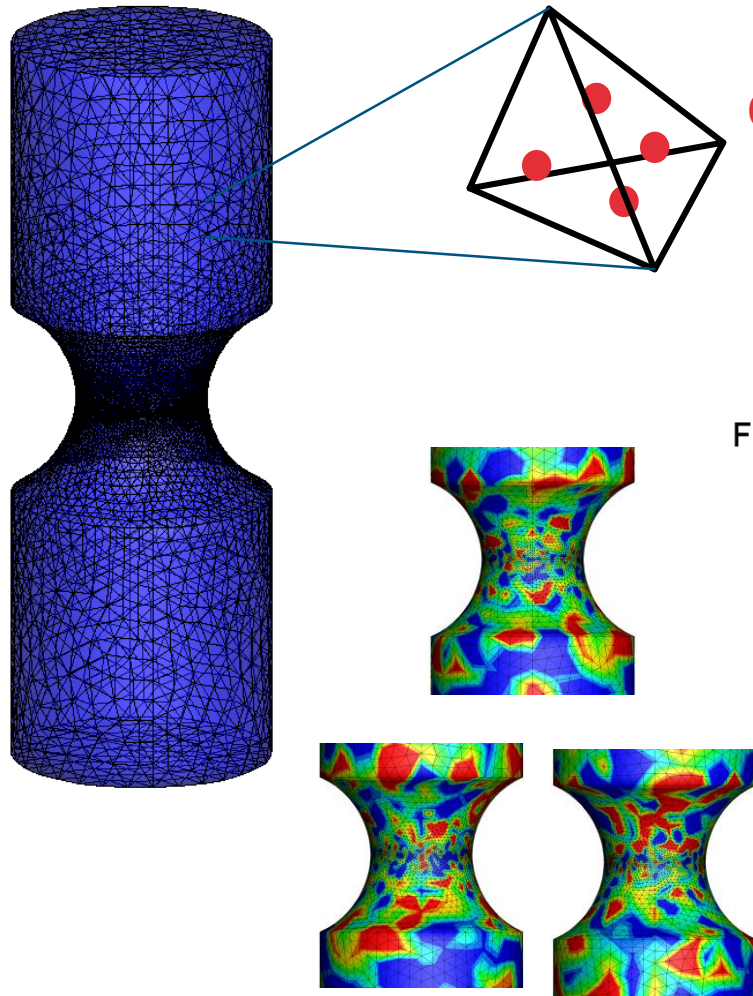


Looking for statistics on particle volume fraction ( $f_0$ )  
-dependent upon sampling volume!

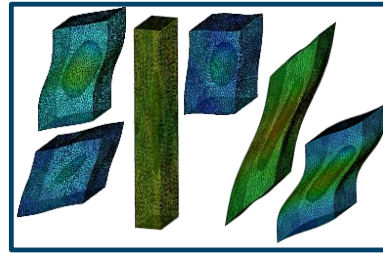
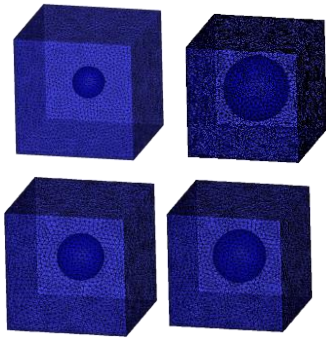




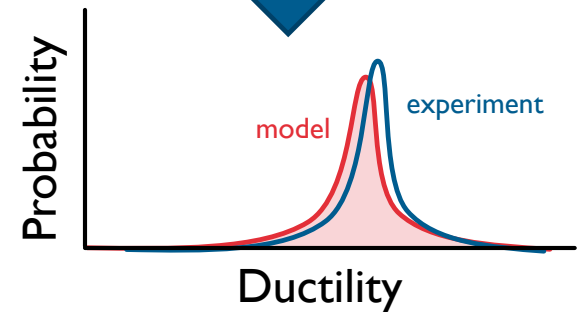
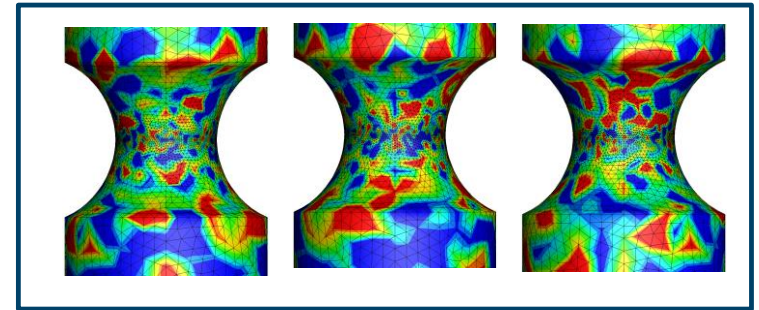
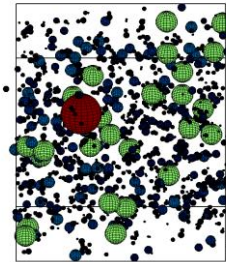
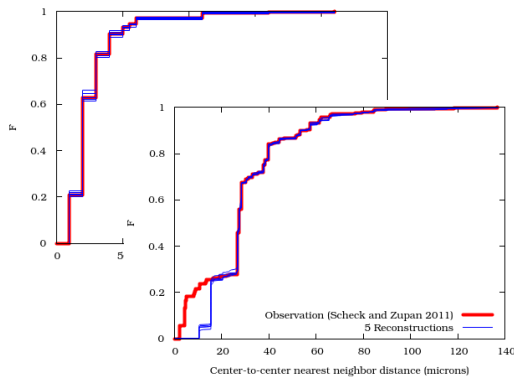
# ASSIGNING LOCAL MICROSTRUCTURE



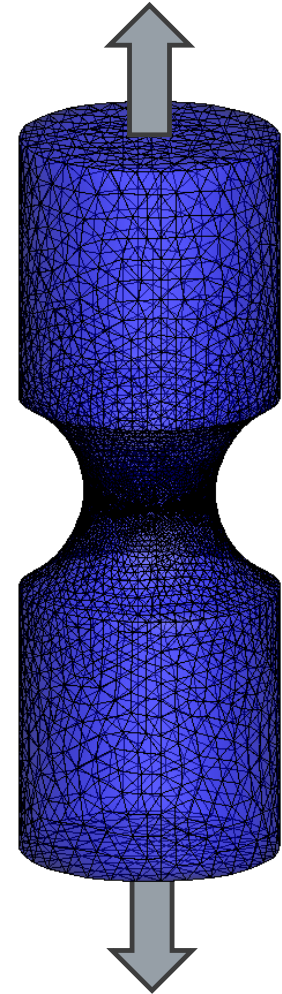
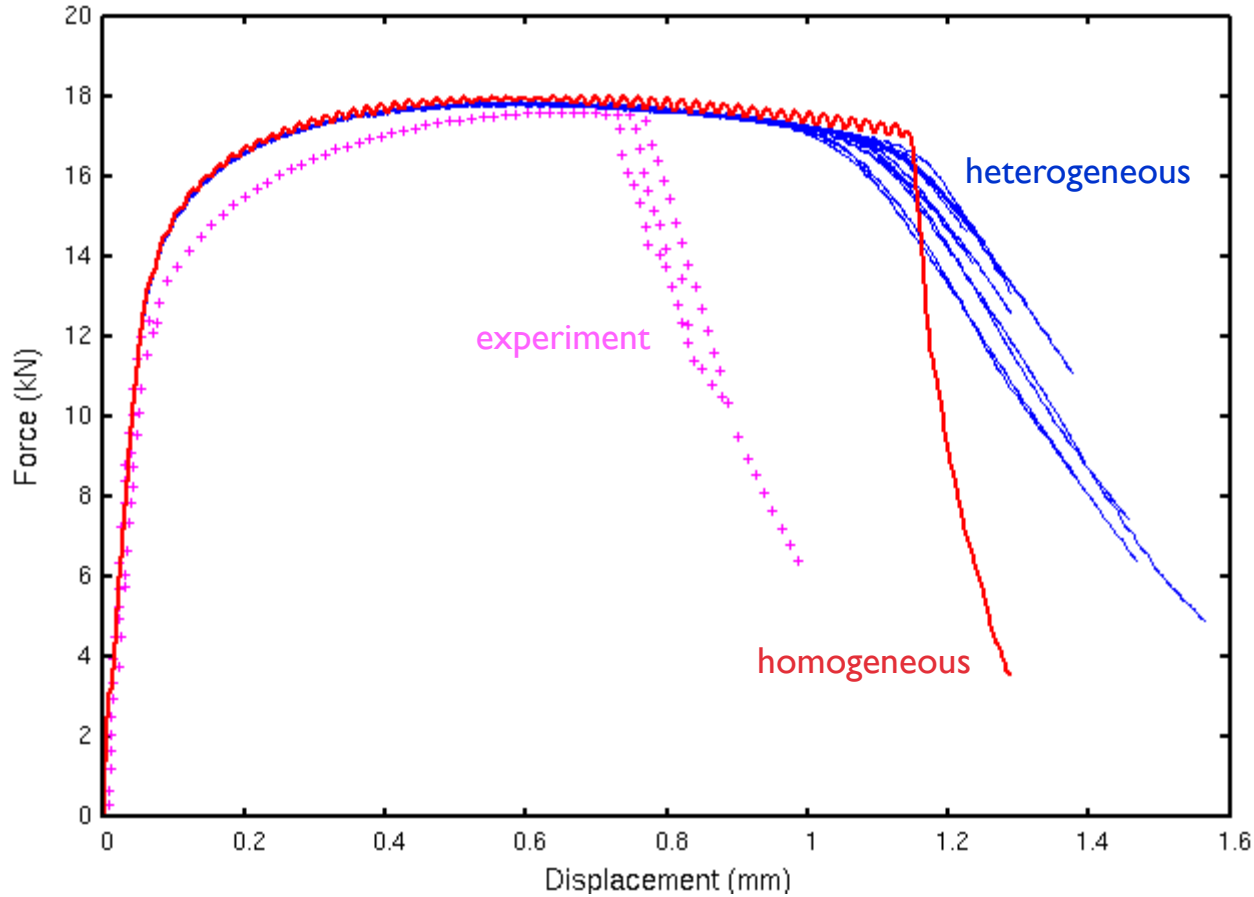
# RECAP ON SEEDING RANDOM MICROSTRUCTURES



Response =  
 $f(\text{microstructure}, \text{loading})$

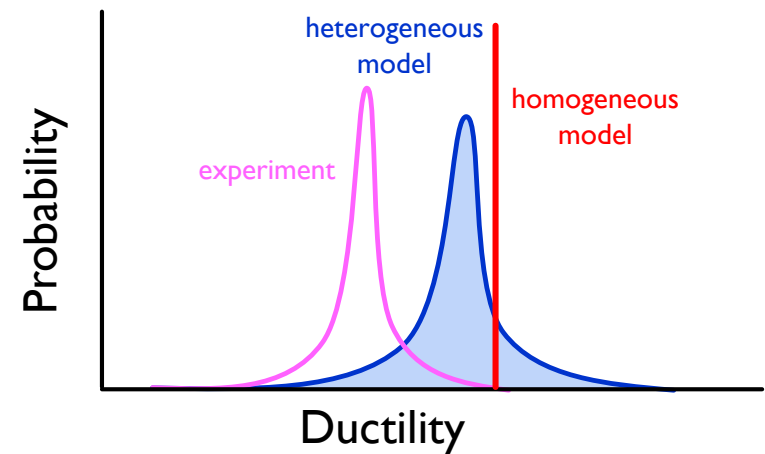


# PRELIMINARY RESULTS





- Failure initiation in a homogeneous material over predicts ductility
- Microstructural heterogeneity leads to macro-scale uncertainty
- Better statistics on microstructure (from observation rather than reconstruction) are needed
- Incorporation of more microstructural features could yield improvements



# THANK YOU!

ARE THERE ANY QUESTIONS?

